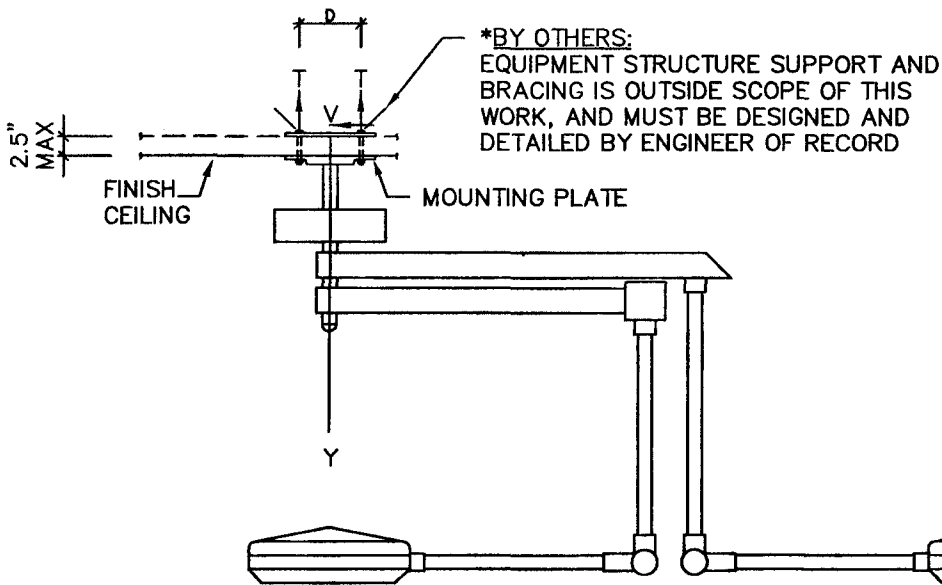


# FIROUZI CONSULTING ENGINEER, INC.

SKYTRON SURGICAL PRODUCTS	DES.	SHEET  <b>1</b>  OF 4 SHEETS
STELLAR SERIES - ST 2319WC FOR SEISMIC ZONE (4), SOIL PROFILE (Sd) NEAR SOURCE FACTOR = 1.5	FCE JOB No.	
	DATE: 6-22-04	

## SEISMIC ANCHORING BOLT DESIGN **ST2319WC**



RENEWAL FEE DUE DATE: 06-30-06

### ELEVATION

1. SCOPE OF WORK: DESIGN OF BOLTS CONNECTING MOUNTING PLATE TO STRUCTURE ONLY.
2. FORCES ARE DETERMINED PER 2001 CALIFORNIA BUILDING CODE – SECTION 1632A, (INCLUDING UP TO DATE REVISIONS) AND HAVE BEEN FACTORED TO REPRESENT WORKING DESIGN LOADS, NOT ULTIMATE
3. FORCES ARE MAXIMUMS AND OCCUR WHEN EQUIPMENT IS MOVED TO ITS MOST ECCENTRIC POSITION.
4. PROVIDE CEILING STRUCTURE DESIGNED AND DETAILS TO SUPPORT WEIGHTS AND FORCES SHOWN (BY ENGINEER OF RECORD FOR THE BUILDING)
5. ENGINEER OF RECORD TO DESIGN, DETAIL AND VERIFY STRUCTURE AND/OR EXISTING LIGHT SUPPORT TRACTS TO SUPPORT INDICATED LOADS
6. HORIZONTAL FORCES AND MOMENT MAY OCCUR IN ANY DIRECTION, ACTING AT THE TOP OF MOUNTING PLATE.

# FIROUZI CONSULTING ENGINEER, INC.

SKYTRON SURGICAL PRODUCTS	DES.	SHEET  <b>2</b>  OF 4 SHEETS
STELLAR SERIES - ST 2319WC FOR SEISMIC ZONE (4), SOIL PROFILE (Sd) NEAR SOURCE FACTOR = 1.5	FCE JOB No.	
	DATE: 6-22-04	

## DESIGN CRITERIA:

FORMULA 32A-1:  $F_p = 4.0 C_a I_p W_p$

TABLE 16A-Q :  $C_a = 0.44 N_a = 0.44 * 1.5 = 0.66$  ( For zone 4 & Sd)

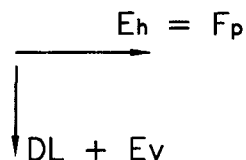
TABLE 16A-K :  $I_a = 1.5$  ( For essential facility)  
 $\therefore F_p = (4.0)(0.66)(1.5)W_p = 3.96 W_p$  (For LRFD)  
 $F_p = 3.96 W_p / 1.4 = 2.83 W_p$  (For ASD)

FORMULA 30A-1:  $E = p E_h + E_v$   
 $E_h = F_p$   
 $p = 1.0$  (FOR COMPONENT)

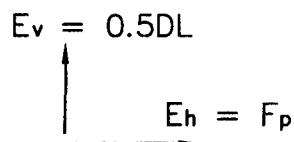
$$\begin{aligned} E_v &= (0.5) C_a I_p W_p \\ &= (0.5)(0.66)(1.5) W_p = 0.5 W_p \text{ (For LRFD)} \\ &= 0 \quad \text{(For ASD)} \end{aligned}$$

SECTION 1630A.11:  $E_v = (0.7) C_a I W_p$   
 $= (0.7)(0.66)(1.5) / 1.4 = 0.5 W_p$  (For ASD) [NET UPLIFT FORCE]

## LOAD COMBINATION CASE A



## LOAD COMBINATION CASE B



BY COMPARISON LOAD, COMBINATION A GOVERNS

# FIROUZI CONSULTING ENGINEER, INC.

SKYTRON SURGICAL PRODUCTS

DES.

SHEET

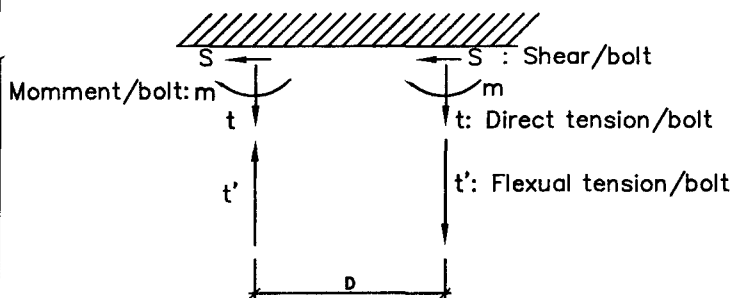
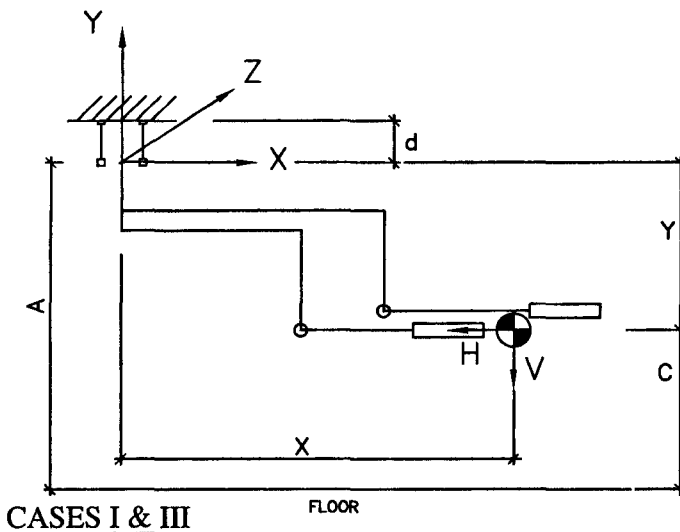
STELLAR SERIES - ST 2319WC  
FOR SEISMIC ZONE (4), SOIL PROFILE (Sd)  
NEAR SOURCE FACTOR = 1.5

FCE  
JOB No.

3

DATE: 6-22-04

OF 4 SHEETS



A: MAX FLOOR TO MOUNTING PLATE  
DISTANCE

$$A = 10'-0" = 120"$$

$$C = 80"$$

Vd : Dead Load (=DL)

Ve : Vertical Seismic Load (=Ev)

He : Horizontal Seismic Load (=Eh)

**CASE I (FIXTURE AT HIGH POSITION)**

$$d = 2.5"$$

$$D = 9.5"$$

$$Vd = 72 + 119 = 191 \#$$

$$Y = (120 - 80) = 40.0"$$

$$X = (70.5 \times 72 + 78.3 \times 119) / 191 = 75.4"$$

$$Ve = 0.50 \times 191 = 94.5 \#$$

$$He = 2.83 \times 191 = 540.3 \#$$

$$S = 540.3 / 4 = 135.1 \#$$

$$t = (191 + 94.5) / 4 = 71.4 \#$$

$$\text{Total } M_{zz} = (191 + 94.5) \times 75.4 + 540.3 \times 40 = 43129 \text{ " \#}$$

$$t' = 43129 / (9.5 \times 2) = 2270 \#$$

$$m = 135.1 \times 2.5 = 338 \text{ " \#}$$

**CASE II (FIXTURE AT LOW POSITION)**

$$d = 2.5"$$

$$D = 9.5"$$

$$Vd = 191 \#$$

$$Y = [(40.0 + 35.3) \times 72 + (40.0 + 35.3) \times 119] / 191 = 75.3"$$

$$X = (35.3 \times 72 + 43 \times 119) / 191 = 40.1"$$

$$Ve = 0.50 \times 191 = 94.5 \#$$

$$He = 2.83 \times 191 = 540.3 \#$$

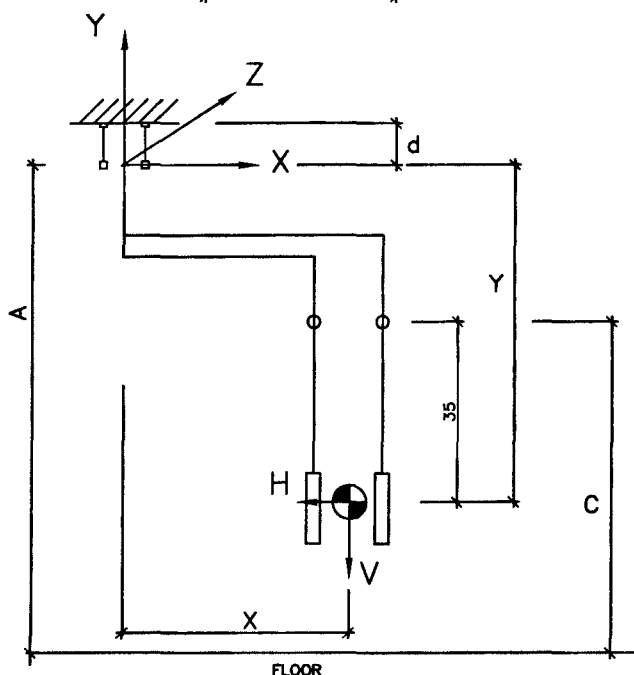
$$S = 540.3 / 4 = 135.1 \#$$

$$t = (191 + 94.5) / 4 = 71.4 \#$$

$$\text{Total } M_{zz} = (191 + 94.5) \times 40.1 + 540.3 \times 75.3 = 52131 \text{ " \#}$$

$$t' = 52131 / (9.5 \times 2) = 2744 \#$$

$$m = 135.1 \times 2.5 = 337.7 \text{ " \#}$$

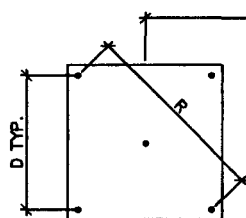


# FIROUZI CONSULTING ENGINEER, INC.

SKYTRON SURGICAL PRODUCTS	DES.	SHEET  <b>4</b>  OF 4 SHEETS
STELLAR SERIES - ST 2319WC FOR SEISMIC ZONE (4), SOIL PROFILE (Sd) NEAR SOURCE FACTOR = 1.5	FCE JOB No.	
	DATE: 6-22-04	

## CASE III (Same As CASE I, Lateral Forces Applied Diagonally To Mounting Plate)

$d = 2.5"$   
 $D = 13.4"$   
 $V_d = 191 \#$   
 $Y = 40.0"$   
 $X = 75.4"$   
 $V_e = 0.50 \times 191 = 94.5 \#$   
 $H_e = 2.83 \times 191 = 540.3 \#$   
 $S = 540.3 / 4 = 135.1 \#$   
 $t = (191 + 94.5) / 4 = 71.4 \#$   
 $\text{Total } M_{zz} = (191 + 94.5) \times 75.4 + 540.3 \times 40 = 43129 \text{ "}\#$   
 $t' = 43129 / (13.4 \times 1) = 3210 \#$   
 $m = 135.1 \times 2.5 = 337.7 \text{ "}\#$



C.G.  
 CASES I & II  
 $D = 9.5"$

## CASE IV

(Same As CASE II, Lateral Forces Applied Diagonally To Mounting Plate)

$d = 2.5"$   
 $D = 13.4"$   
 $V_d = 191 \#$   
 $Y = 75.3"$   
 $X = 40.1"$   
 $V_e = 0.50 \times 191 = 94.5 \#$   
 $H_e = 2.83 \times 191 = 540.3 \#$   
 $S = 540.3 / 4 = 135.1 \#$   
 $t = (191 + 94.5) / 4 = 71.4 \#$   
 $\text{Total } M_{zz} = (191 + 94.5) \times 40.1 + 540.3 \times 75.3 = 52131 \text{ "}\#$   
 $t' = 52131 / (13.4 \times 1) = 3880 \#$  GOVERNS  
 $m = 135.1 \times 2.5 = 337.7 \text{ "}\#$

C.G.  
 CASES III & IV  
 $R = 9.5(2)^{0.5} = 13.4"$

CHECK 3/4" DIA. A307 BOLTS:

ALLOWABLE TENSION: 8,800 #  
 ALLOWABLE SHEAR: 4,400 #

$S = 3.14 \times d^3 / 32 = 3.14 \times (0.75)^3 / 32 = 0.04 \text{ "}$   
 $f_b = 337.7 / 0.04 = 8157 \text{ PSI}$   
 $F_b = 0.75 \times 36000 = 27000 \text{ PSI}$

$f_v / F_v + f_t / F_t + f_b / F_b = 0.03 + 0.44 + 0.30 = 0.77 < 1.0$  OK

USE 3/4" DIA. A307 BOLTS